DEPARTMENT OF NATIONAL DEVELOPMENT

BUREAU OF MINERAL RESOURCES, GEOLOGY AND GEOPHYSICS

Record No. 1969 / 146

053371



Jervis Bay Reconnaissance Seismic Survey, ACT 1969

by

F. J. Taylor

The information contained in this report has been obtained by the Department of National Development as part of the policy of the Commonwealth Government to assist in the exploration and development of mineral resources. It may not be published in any form or used in a company prospectus or statement without the permission in writing of the Director, Bureau of Mineral Resources, Geology & Geophysics.



Record No. 1969 / 146

Jervis Bay Reconnaissance Seismic Survey, ACT 1969

by

F. J. Taylor

The information contained in this report has been obtained by the Department of National Development as part of the policy of the Commonwealth Government to assist in the exploration and development of mineral resources. It may not be published in any form or used in a company prospectus or statemen without the permission in writing of the Director, Bureau of Mineral Resources, Geology and Geophysics.

CONTENTS

	SUMMARY				
1.	INTRODUCTION	1			
2.	GEOLOGY	1			
3.	METHODS AND EQUIPMENT	2			
4.	RESULTS	2			
5•	CONCLUSIONS	3			
6.	ACKNOWLEDGEMENTS	4			
7•	REFERENCES	4			
	APPENDIX A	5			
	TABLE I	5			

ILLUSTRATIONS

Plate 1.	Locality	y map		(Drawing No	. I56/B5 - 3)
Plate 2.	Traverse	e plan,	site JS1		(I56/B5-4)
Plate 3.	Traverse	e plan,	site JS2	2	(I56/B5 - 5)
Plate 4.	Seismic	cross-	sections,	Traverses J, K, and R	(156/B5-8)
Plate 5.	11	**	. 11	Traverses L and M	(156/B5 - 9)
Plate 6.	tt	11	11 1	Traverses N and O	(156/B5-10)
Plate 7.	11	11	",	Traverses P and Q	(I56/B5 - 11)
Plate 8.	• 11	11	",	Traverse H	(I56/B5 - 12)
Plate 9.	**	11	",	Traverses S, T, and X	(I56/B5013)
Plate 10.	11	11	, n	Traverses U, V, and W	(I56/B5-14)

Record 1969/146

SUMMARY

A seismic refractior survey was carried out for the Australian Atomic Energy Commission at Jervis Bay, ACT during July and August 1969 to investigate two proposed sites for a nuclear power station. The two sites are Sandy Beach (JS1), and Murrays Beach (JS2) (Plate 1). Additional work was carried out in the vicinity of Lake Windermere for the Engineering Section of the Geological Branch of the Bureau of Mineral Resources. Although the location of the traverses around Lake Windermere has been included in Plate 1 the results and conclusions of this work will not be included in this report but will await further geophysical work before being incorporated in a separate report.

The bedrock at the two sites consists of Permian sandstone with a seismic velocity varying between 7000 and 15,000 ft/s. The overburden consists almost wholly of sand and weathered sandstone and attains a maximum thickness of 200 feet.

The ideal site for the nuclear power station is one where the upper limit of hard rock lies around 10 feet above sea level. An area of about 1000 feet square is required at this altitude. The upper limit of rock on the eastern end of site JS1 is around this required level but it is doubtful whether the area is large enough. A more promising area is the western side of site JS2 where the sand weathered sandstone boundary appears to be around sea level and the area concerned is quite large.

INTRODUCTION

The Commonwealth Government in conjunction with the State Government of New South Wales wished to investigate the feasibility of building a power station on Commonwealth Territory at Jervis Bay. The foundations of the principal building housing the nuclear reactor must be on rock of suitable strength approximately 10 feet above sea level, the elevation being critical since an immense amount of sea water must be pumped through the plant in order to cool the reactor. It is proposed to channel the coolant sea water through a trench 3000 to 4000 feet in length excavated to 30 feet below sea level.

In response to a request from the Australian Atomic Energy Commission and the Electricity Commission of New South Wales a geophysical survey was conducted by the Geophysical Branch of BMR to determine the depth to fresh rock and the nature of the overburden. The survey was carried out during July and early August 1969, by a geophysical party comprising F.J. Taylor (party leader), P.C. Pollard (geophysicist), A.W. Schuett (Technical Assistant), D. Tarlinton (Technical Assistant) and T. Kimber (Drafting Officer). The supervising geophysicist was Dr E.J. Polak, who with R.J. Whiteley (geophysicist) assisted during the early part of the survey. Field assistants were provided by the Australian Atomic Energy Commission.

The terms "bedrock" and "overburden" as used in this report refer to the deepest refractor detected and the sand and weathered material above this refractor respectively.

2. GEOLOGY

The following geological summary was provided by M.J. Jackson of the Geological Branch of BMR. Plate 1 shows geology mapped by W.J. Perry and J.M. Dickins also of the Geological Branch. The Territory of Jervis Bay consists of gently-dipping, well jointed Permian sandstone (Jervis Bay Sandstone) overlain in places by unconsolidated Quaternary beach and dune sands, which contain lagoonal marsh deposits in some areas. The Jervis Bay Sandstone is generally a medium to coarse-grained, light-grey, massively-bedded sandstone, but silty layers and conglomeratic horizons occur at many levels in the succession. The fresh sandstone can be excavated only by heavy drilling and blasting, and it should provide strong fundations. Dolerite dykes and sills, weathered in places to pure kaolinitic clay, have intruded the sandstone in several localities. Ferruginous gravels occur on an irregular surface of sandstone in the north-west of the Territory.

The fine-grained Quaternary quartz sands range in colour from white to orange, and in thickness from a few feet to 200 feet. The deposition of these sands during the Quaternary Period was controlled largely by platforms and irregularities in the underlying sandstone. Hence, an evaluation of sand thicknesses and depths to bedrock requires extensive geophysical exploration.

3. METHODS AND EQUIPMENT

The depth to bedrock and the nature of the overburden were investigated using 24-channel SIE refraction equipment with TIC 20-Hz geophones. An oil filled bay cable with Hall-Seers MP-8E hydrophones were used for the water work. The well known and established "reciprocal geophone method" (Heiland, 1946) was used in conjunction with short weathering spreads (200 feet) to obtain all seismic data presented in this report. The normal geophone spread consisted of 23 geophones spaced 50 feet apart, and continuous coverages over all traverses were obtained using this spread. This spread gives depths to bedrock while the short weathering spreads placed every 1000 feet give information on the overburden.

The Electricity Commission of New South Wales contracted to have holes drilled on both sites using an auger drill and a diamond drill. Core samples taken from several diamond-drill holes were tested in the BMR laboratories and the specific gravity, seismic velocity (longitudinal waves), and compressive strength of several samples are shown in Table 1.

The seismic velocity was obtained using Cawkell ultrasonic equipment while the compressive strength was computed from an empirical formula relating seismic velocity to compressive strength (Wiebenga & Manganwidjoyo, 1960). This formula is valid for dry rocks with seismic velocities in excess of $6000 \, \text{ft/s}$.

A total of 40,000 feet of traverses including 7000 feet of water traverses was completed on sites JS1 and JS2.

4. RESULTS

Plates 1, 2, and 3 show the location of the geophysical traverses while the seismic cross-sections are shown in Plates 4 to 10. The symbols used in these plates are explained in the legend attached to each plate. The elevation is expressed in feet and the point marked "O" represents mean high water at St Georges Basin.

Both sites have been interpreted as consisting essentially of four layers as outlined below:

- (1) The first layer consists of dry to moist sand with a seismic velocity between 1000 to 2300 ft/s. The thickness of this sand varies between 3 and 100 feet.
- (2) A second layer with a velocity between 3000 and 4000 ft/s is again interpreted as sand or clay but more compacted than that in the uppermost layer and possibly bonded by iron compounds.
- (3) Those regions having velocities between 5000 and 9000 ft/s are interpreted as sandstone in various stages of weathering. Sandstone with velocities above 7500 ft/s, although weathered, would probably be quite suitable for fundations; it is probably the upper limit of velocities in sandstone that can be excavated without use of explosives.

(4) Finally the highest velocities measured, between 11,000 and 15,000 ft/s are interpreted as fresh sandstone. The depth to this region varies from 40 to 150 feet.

There are some variations from the four-layer structure outlined above. The velocity of 5000 ft/s measured along Traverses R and K on site JS1 is due to water-saturated sand. Both these traverses are close to the high water mark along Sandy Beach. Also the velocity of 4000 ft/s measured along Traverse J near spread 11 and spread 19 appears to be due to ferruginous sands situated within a few feet of the surface. It would appear that material of this nature is responsible for the shallowness of auger holes A5, A6, A7, and A8 on site JS2. That is to say although this material has rather a low velocity (4000 ft/s) it appears to be too hard for the auger drill. This idea tends to be confirmed by the measured velocity of a core from hole JS1/D3. A quite solid core from a depth of 25 feet gave a velocity of only 3280 ft/s, but the auger refused to drill at 23 feet at this same location. Hence poor correlation between auger holes and "seismic" depths need not mean that either one or the other is incorrect.

The error in depth determination is considered to be less than 20 percent, while the error in the relative depth to bedrock from station to station is considerably less than this. A comparison of the depths obtained by drill holes and the seismic method can easily be made from Plates 4 to 10. Along Traverse J the correlation is quite good. It should be noted here that in the region between spread 15 and spread 11 on Traverse J although the section shows sand (1800 ft/s) all the way to bedrock it is certain that a thin layer of weathered material (about 7000 ft/s) will exist above the bedrock. It must also be remembered that the seismic survey was a reconnaissance survey and that information on the overburden is supplied only every 1000 feet. There is definitely a lack of weathering information along Traverse W at site JS2. Although two weathering spreads were placed along this traverse there appears to be no indication of material with a velocity between 3000 and 4000 ft/s. Traverse W is situated along a ridge, and it is possible that erosion has reduced the thickness of any such material, in which case its detection would become difficult.

5. CONCLUSIONS

The ideal site for the nuclear power station is one where the upper limit of hard rock lies around 10 feet above sea level. The area required at this altitude is approximately 1000 feet square. On site JS1 the eastern end is perhaps the only area approaching the above ideal conditions. Even so it is doubtful whether this area is large enough. On the western end, solid rock extends to as high as 50 feet above sea level and hence the excavation costs in the area may be prohibitive.

On site JS2 the area bounded by Traverses S, T, U, and V appears to be the most suitable area for a site. Along Traverse U the sand/weathered sandstone boundary appears to be around sea level. This boundary rises towards the east and attains a height of about 40 feet above sea level in the vicinity of Traverse V. Hence, providing the

material with velocity 3000 to 4000 ft/s is not too difficult to remove, and it should not be, the excavation costs for this site should not be prohibitive and the actual foundations will not require extensive piledriving.

6. ACKNOWLEDGEMENTS

The members of the seismic party wish to acknowledge the cooperation given by the officers of the Electricity Commission of New South Wales, the Australian Atomic Energy Commission, and the Department of the Interior.

7. REFERENCES

HEILAND, C.A., 1946 - GEOPHYSICAL PROSPECTING, New York, Prentice Hall.

WIEBENGA, W.A. and MANGANWIDJOYO, A., 1960 - Some correlations between rock parameters derived from Wuerker's Annotated Tables.

Trans. Amer. Inst. Engrs. 217

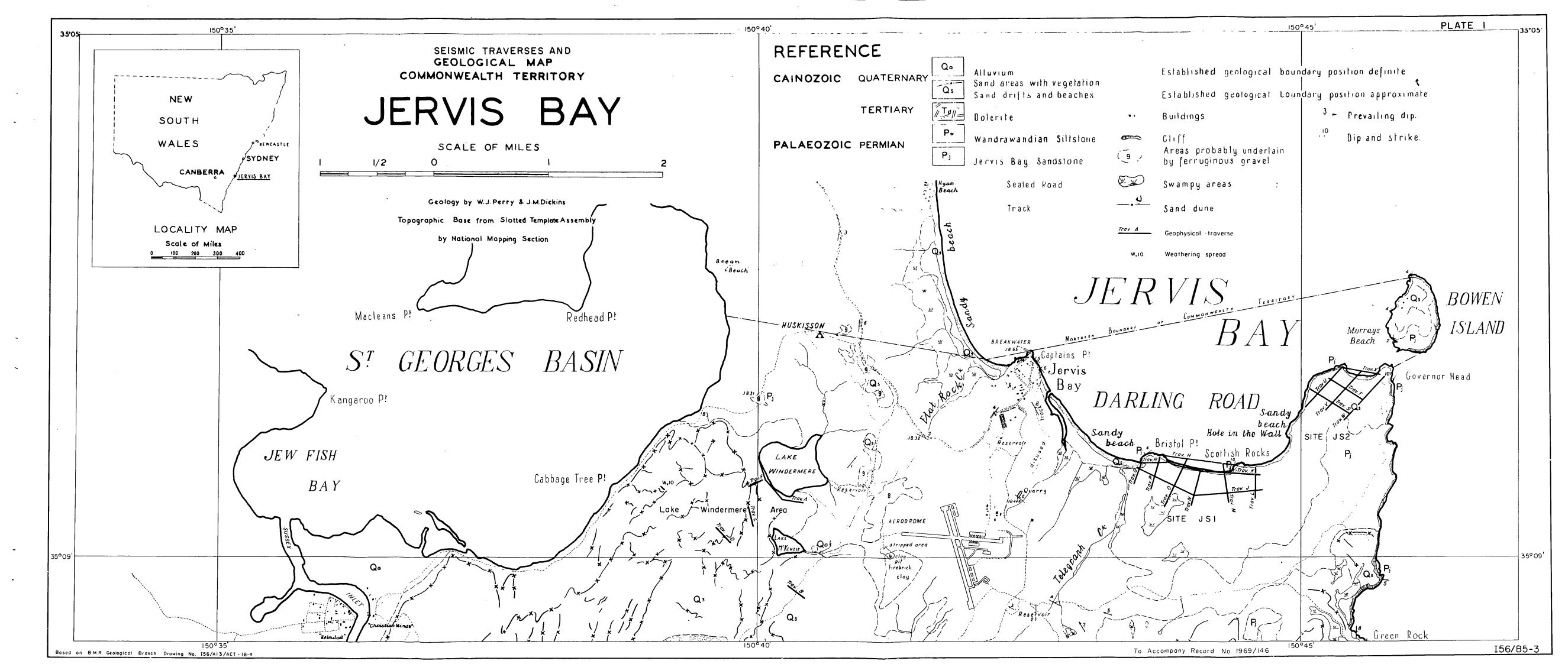
APPENDIX A

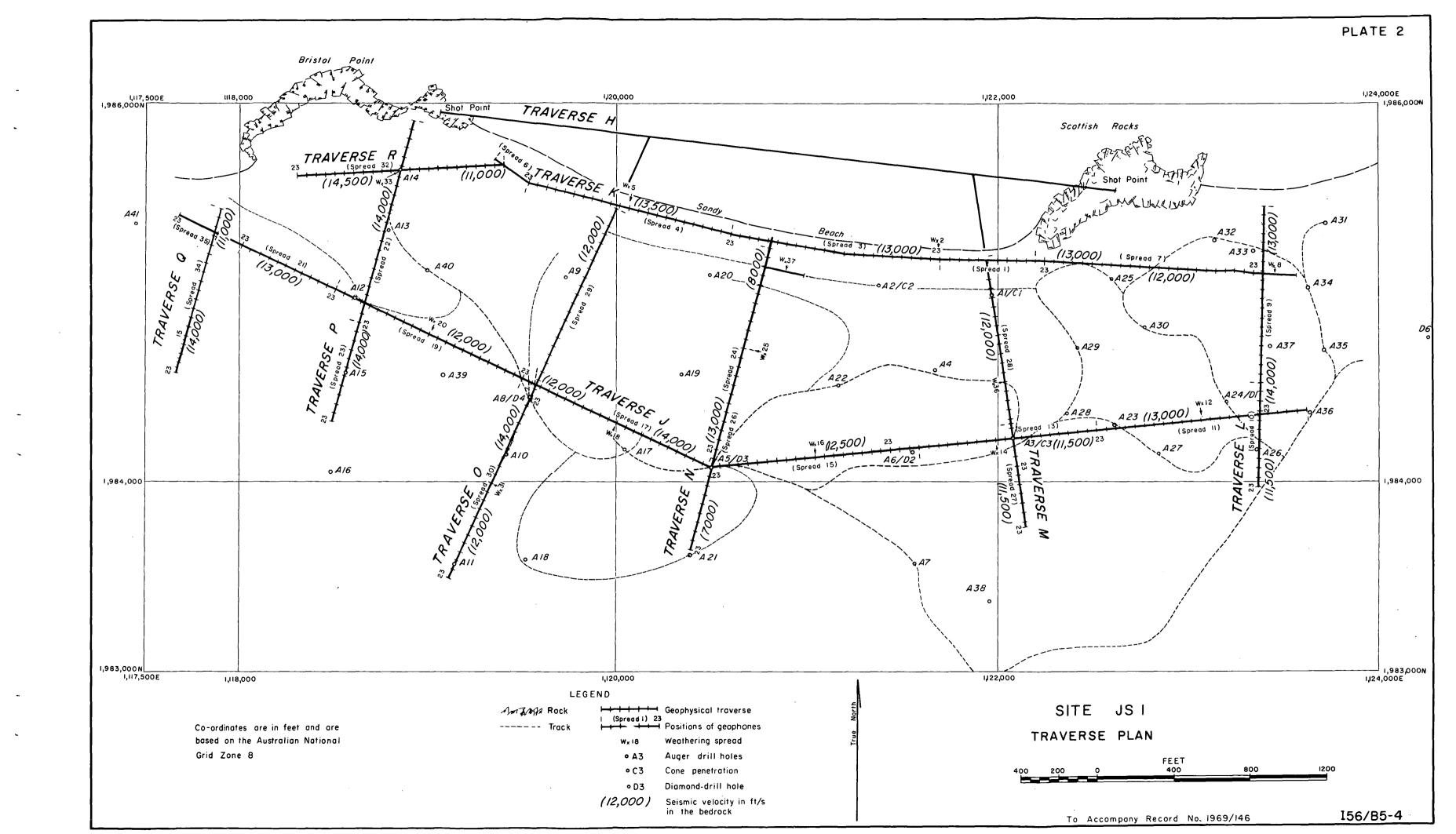
- (1) The zero elevation level used in this report is the mean high-water level of St Georges Basin, Jervis Bay, ACT. This datum is the standard datum adopted by the Department of the Interior for Jervis Bay, ACT.
- (2) The position of the boat for every shot fired for the hydrophone work across Sandy Beach and Murrays Beach is given in BMR drawing No. 156/B5-6. The actual position of the No. 12 hydrophone is 100 feet closer to the shot.
- (3) Survey plans as provided by the surveyer are recorded in BMR drawing No. 156/B5-15.

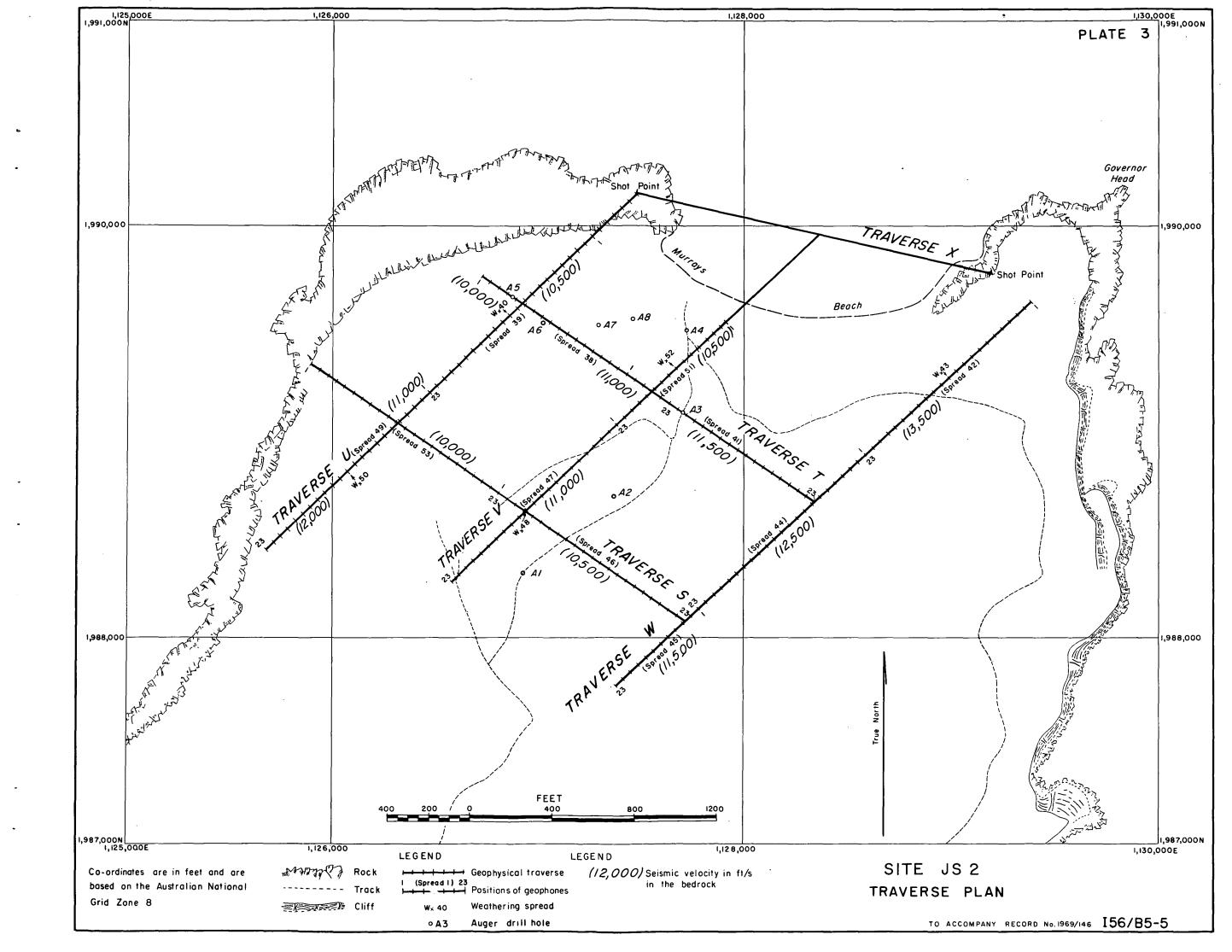
TABLE 1.

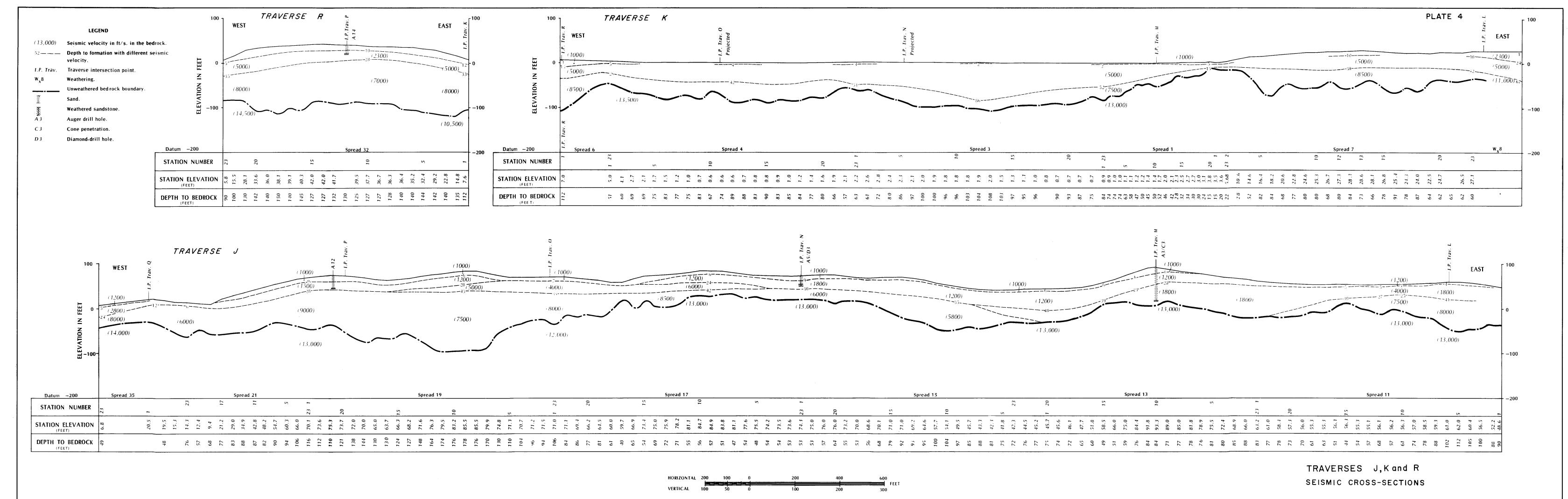
Physical properties of diamond-drill cores

Drill Hole	Depth, ft	Specific gravity	Seismic Velocity ft/s	Compressive strength x 1000 lb/in2
JS1/D1	27.0 - 27.7	2.23	4,050	
	36.6 - 37.1	2.35	8,850	16.93
	61.3 - 61.9	2.44	11,350	22.69
JS1/D3	24.3 - 24.7	2.27	3,280	-
	28.0 - 29.1	2.39	8,650	13.06
1.	52 . 3 - 53.2	2.41	9,960	19.44
JS1/D4	18.4 - 18.9	2.26	Sample broke	under test
	24.0 - 24.9	2.32	5,300	-
	75.2 - 75.9	2.45	10,600	18.38

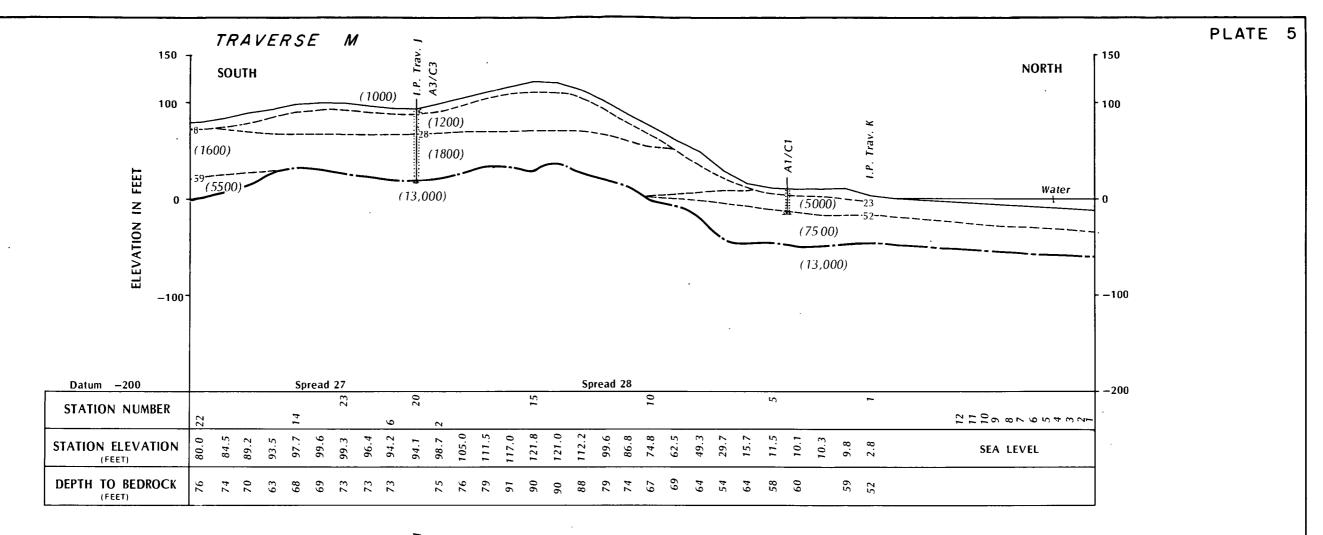


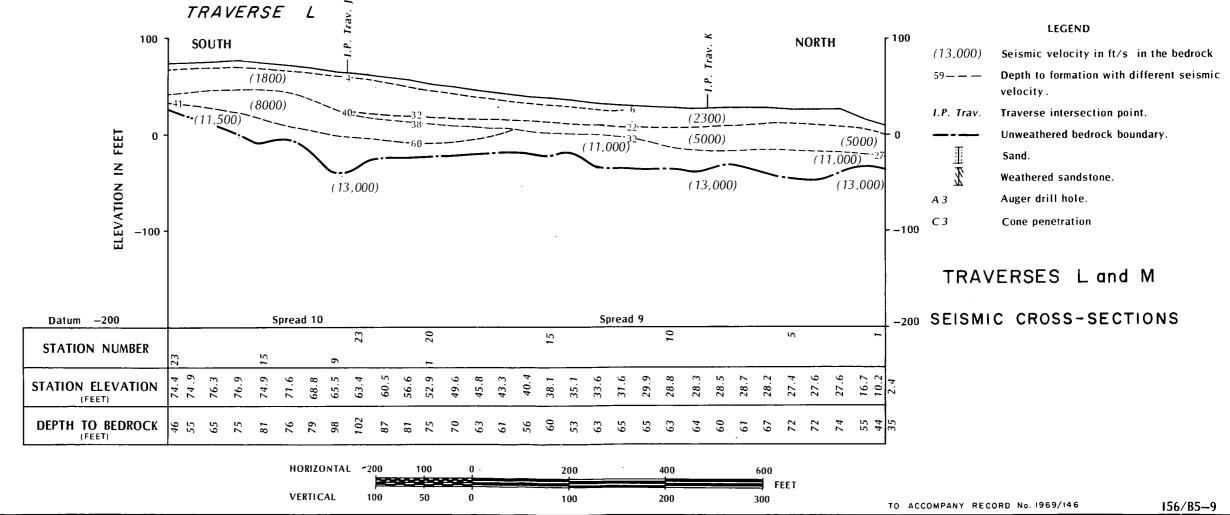


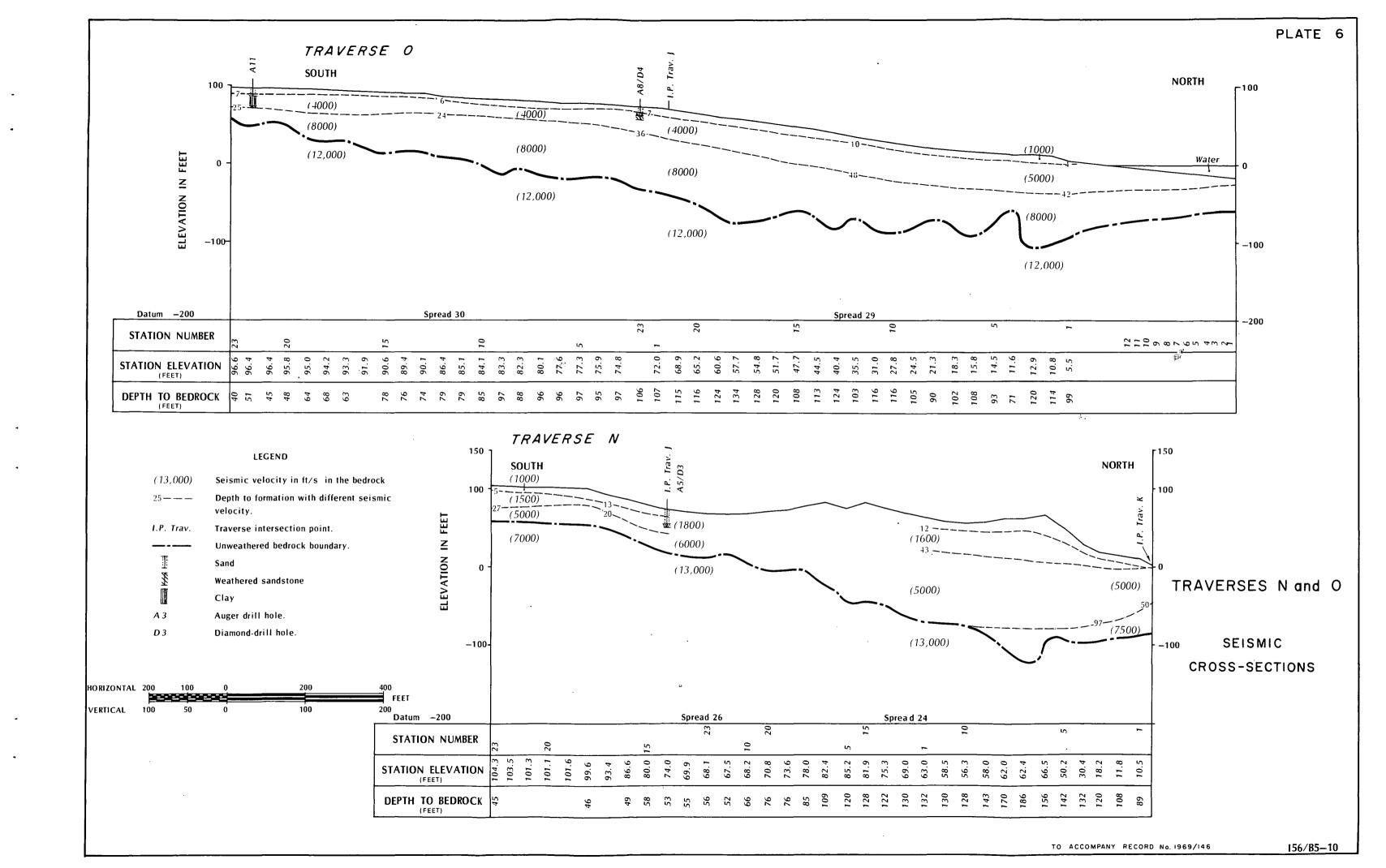




COMPANY RECORD No. 1969/146



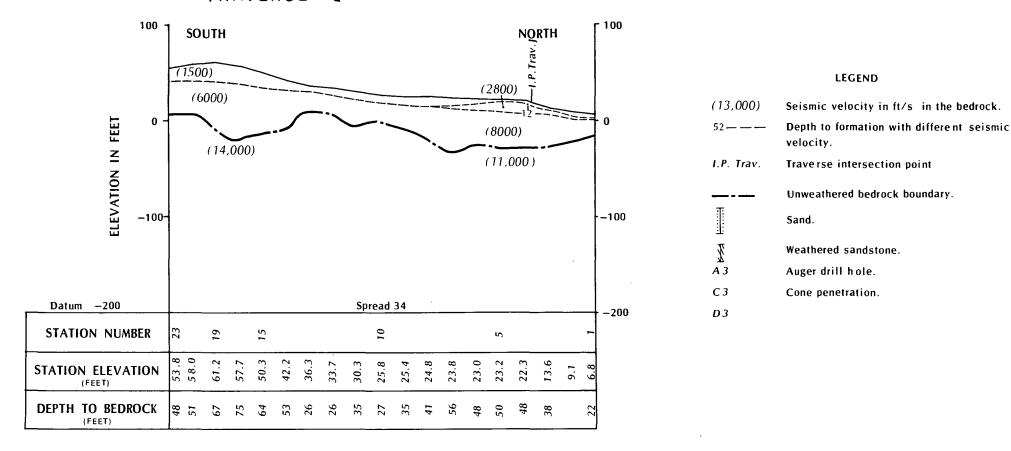


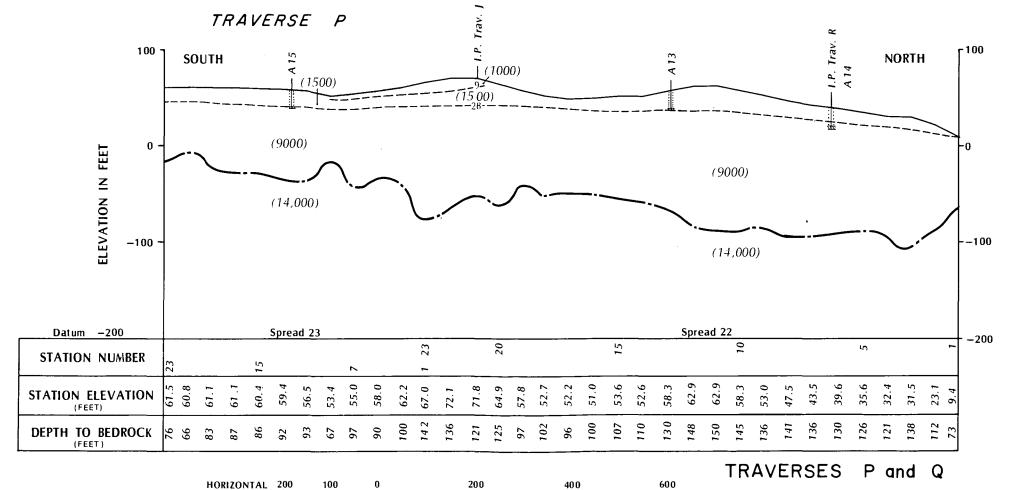


TRAVERSE Q

VERTICAL

100





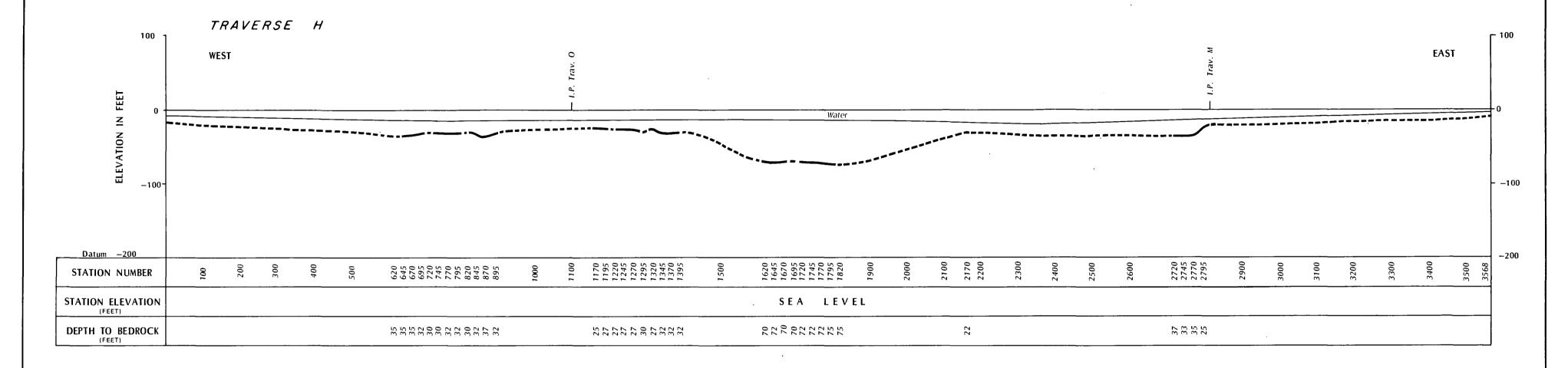
100

200

FEET SEISMIC CROSS-SECTIONS

TO ACCOMPANY RECORD No. 1969/146

I56/B5-11



LEGEND

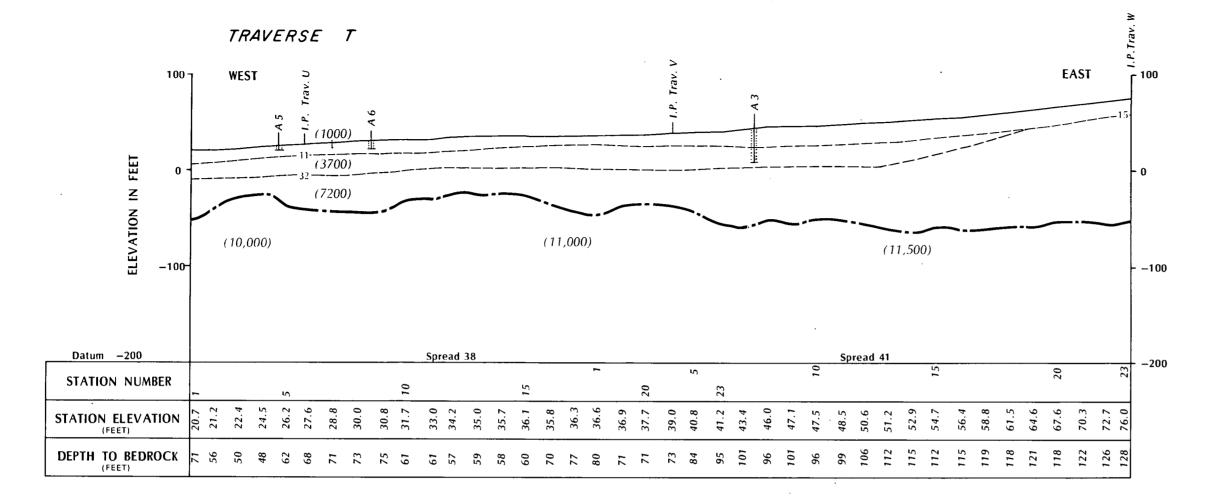
I.P. Trav. Traverse intersection point

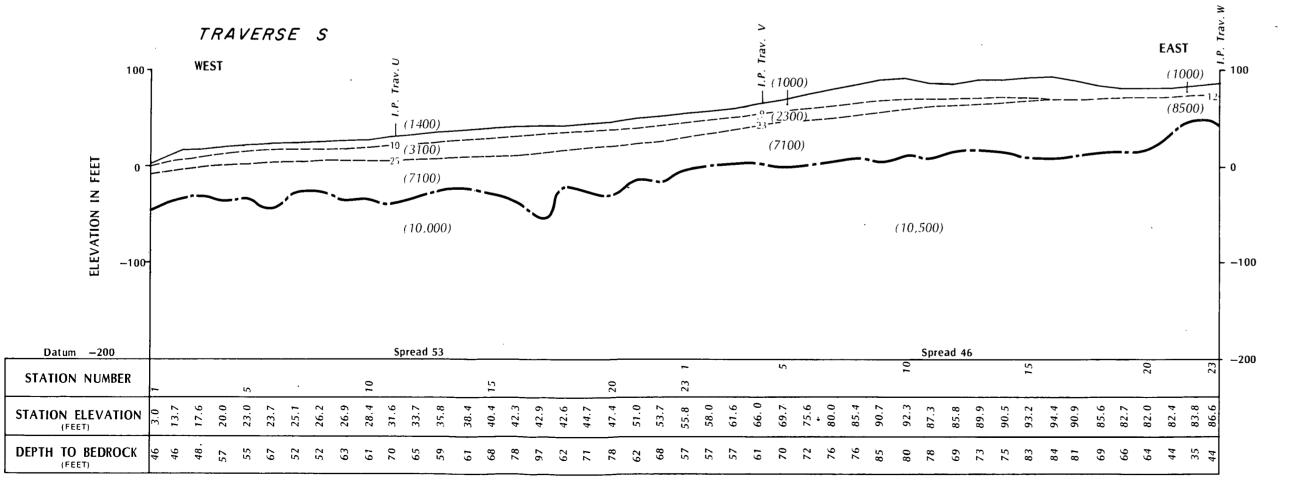
Unweathered bedrock boundary

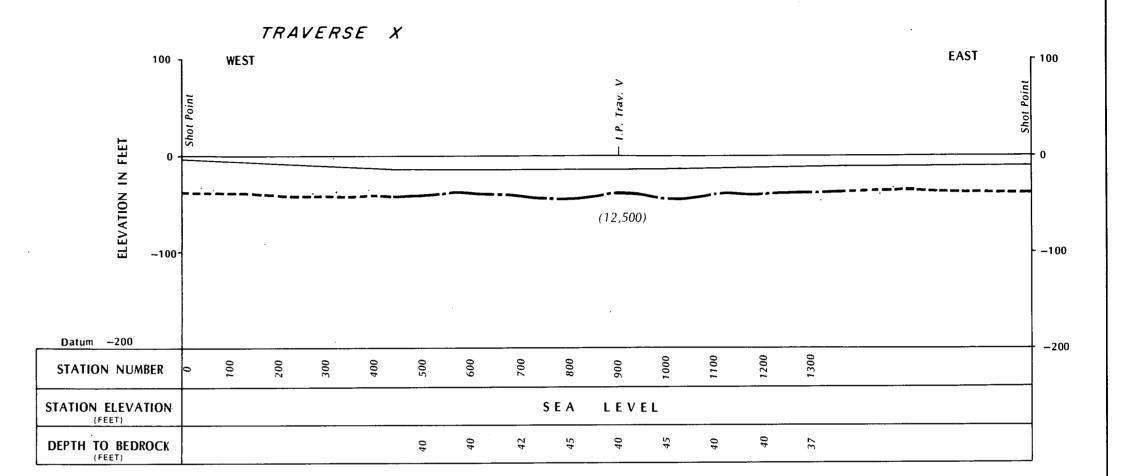
See depth from charts

TRAVERSE H
SEISMIC CROSS-SECTION











Auger drill hole.



PLATE 9

